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## **Technical Specifications**

for

# High Voltage LED Lamp Driver

**DR3062** 

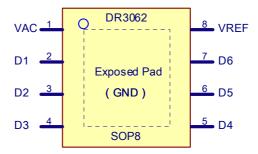
Rev: 3.2A

2012 / 02 / 06



#### **Product Descriptions**

Conventional solutions for LED lighting have some disadvantages such as: (1). Using high current high power LED results in high cost on LED's heatsink, (2). Using bulky transformers occupies considerable PCB space, (3). Using high-voltage electrolytic capacitors yields a short product life due to the aging characteristics of electrolytic capacitors. To cope with the above mentioned problems, ICTI came up with a patented solution without using high-voltage electrolytic capacitors, bulky transformers and high-current LEDs. This solution can greatly reduce the number of external components and save a lot of PCB space.



Top-View of SOP-8 Package





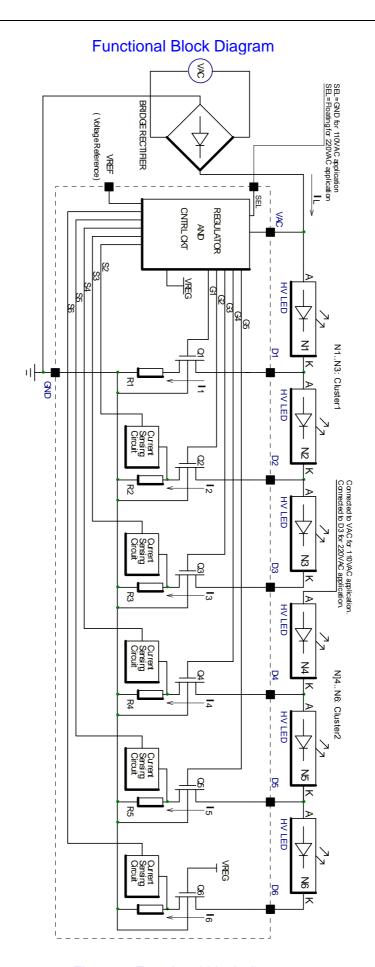


Figure 1: Functional block diagram



### Pin Definitions

Din Nome	Descriptions	Pin number			
Pin Name	Descriptions	SOP8-110	SOP8-220		
VAC	Rectified AC Power	1	1		
GND	Power and Signal Return	Exposed Thermal Pad (bottom)	Exposed Thermal Pad (bottom)		
SEL	<ul><li>Bonding option</li><li>Connected to GND for 110VAC application.</li><li>Floating for 220VAC application.</li></ul>	Internally connected to GND	Internally un-connected		
VREF	External Reference Voltage Globally sets the driving currents	8	8		
D1	1 <sup>st</sup> driver/220VAC (1 <sup>st</sup> driver of cluster1 / 110VAC)	2	2		
D2	2 <sup>nd</sup> driver/220VAC (2 <sup>nd</sup> driver of cluster1 /110VAC)	3	3		
D3	3 <sup>rd</sup> driver/220VAC (3 <sup>rd</sup> driver of cluster1 /110VAC)	4	4		
D4	4 <sup>th</sup> driver/220VAC (1 <sup>st</sup> driver of cluster2 /10VAC)	5	5		
D5	5 <sup>th</sup> driver/220VAC (2 <sup>nd</sup> driver of cluster2 /110VAC)	6	6		
D6	6 <sup>th</sup> driver/220VAC (3 <sup>rd</sup> driver of cluster2 /110VAC)	7	7		

Maximum Rating
Ta=25℃, unless otherwise specified

Parameter	Description		Max	Unit	
Storage temperature		-40	125	C	
Operating temperature		-40	125	C	
Operating voltage	50 / 60Hz	-	350	Vrms	
Leakage current ( D1 ~ D6 )	VREF = 0V, V(D1D6) = 40VDC	-	0.1	uA	
Sustained voltage ( D1 ~ D6 )	VREF = 0V	-	500	Volt	
Driving capability	Instantaneous power ( transient voltage x transient current )	-	4.0	Walt	
( D1 ~ D6 )	Average power	-	0.4	Walt	
External reference voltage (VREF)	DC voltage	-0.3	20	Volt	
Operation mode select (SEL)		-0.3	9	Volt	
Thermal resistance ( RθJA)	SOP8 Package	35	-	.c\M	
Floatro Statio Diochargo (FSD)	human body mode	+/-1200V, Class 1C			
Electro-Static Discharge (ESD)	machine mode	+/-300V, Class M3			
Surge test at the phase of 90°		500	-	Volt	
Latch-up	> 150mA)	Class I, Level A			



### **Electrical Characteristics**

Test conditions: Ta=25℃, VAC=220VAC (rectified), u nless otherwise specified.

Parameter	Symbol	Description	Min	Тур	Max	Unit
Supply voltage	VAC	220VAC application (SEL=floating) [1] [2]	0	220	280	Vrms
(after rectification)	VAC	110VAC application (SEL=GND) [1] [2]	0	110	150	Vrms
Supply current	IDC	V(VAC) = 40VDC, VREF=18VDC	ı	0.1	0.2	mA
Duissing assument	ID1	VREF = 18VDC	16	18	20	mA
Driving current	ID2~6	VREF =18VDC	32	36	40	mA
Temperature coefficient	TC	VREF =18VDC	-	-0.3	-	%/℃
Leakage current	lleak	VREF = 0VDC, V(D1~ D6) =40VDC	ı	ı	0.1	uA
Input impedance of VREF terminal	ZIN		100	-	-	МΩ
Over voltage VOVP protection		Terminal voltage of D6 [3]	100	120	140	Volt
Over voltage response time tOVP			-	-	0.1	uS
Threshold of current sensing circuit	ISW		-	10	-	mA



#### Theory of Operation

The high voltage LED lamp driver, DR3062, has six current limiting drivers from D1 to D6, in which D2 to D6 has an associated current sensing circuit. For 220VAC application, if the current flowing through D2 is detected, D1 driver will be turned off; if the current flowing through D3 is detected, D1, D2 will be turned off; if the current flowing through D4 is detected, D1, D2, D3 will be turned off; if the current flowing through D6 is detected, D1, D2, D3 and D4 will be turned off; if the current flowing through D6 is detected, D1, D2, D3, D4 and D5 will be turned off. For 110VAC application, if the current flowing through D2/D5 is detected, D1/D4 driver will be turned off; if the current flowing through D3/D6 is detected, D1/D3, D2/D4 will be turned off; The above mentioned turn-on-off sequence is implemented by a logic control circuit. The current limiting driver and its associated current sensing circuit are shown in Figure 2; the timing diagram of the logic control circuit is shown in Figures 3 and 4.

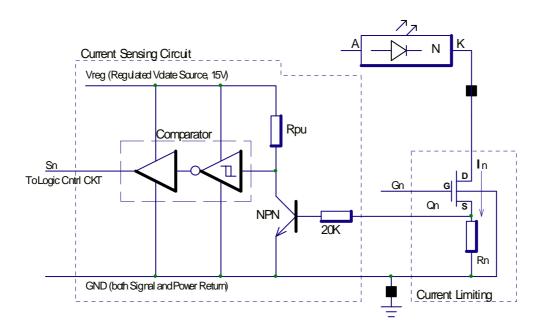


Figure 2: Current limiting driver and current sensing circuit

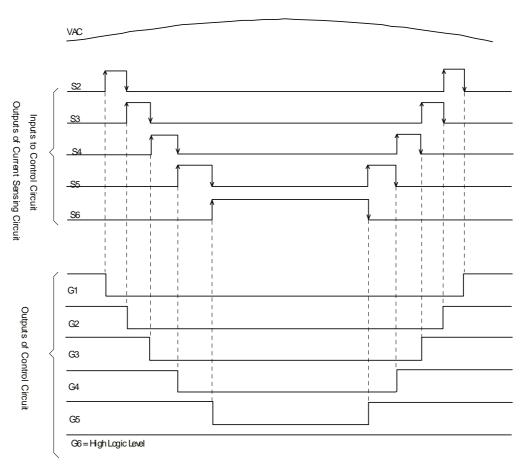


Figure 3: Timing diagram of logic control circuit for 220VAC application

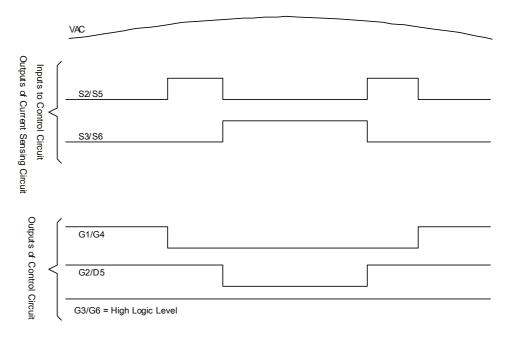


Figure 4: Timing diagram of logic control circuit for 110VAC application



#### **Driving Current Setting**

The external reference, VREF, applied to DR3062 is a reference for its internal regulator. The output voltage of the internal regulator is applied to the logic control circuit; that means, the gate voltage of the current driving MOSFET, G1 ~ G6, is proportional to VREF. Therefore, adjust the external reference voltage, VREF, will change the driving current as shown in Figure 5.

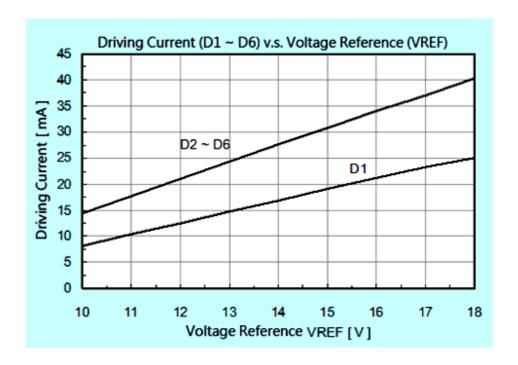


Figure 5: Driving currents, I(D1~D6), v.s. VREF with (V(D1..D6)=40VDC

As the VREF terminal will be pulled to GND level when surge protection circuit is activated, a resistor of  $10K\Omega$  must be connected between the VREF terminal and the externally applied voltage reference.



#### **Current Limiting Driver**

The current limiting driver can supply constant current as the applied voltage to the driver terminal is over 20VDC. Figure 6 shows the behavior of the current limiting driver D1, Figure 7 shows the behaviors of the current limiting drivers D2 to D6.

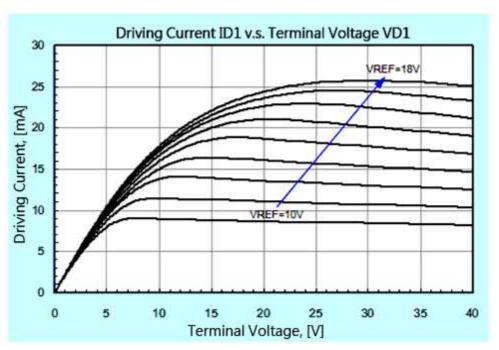


Figure 6: Driving current v.s. driver terminal voltage (I(D1) v.s. V(D1))

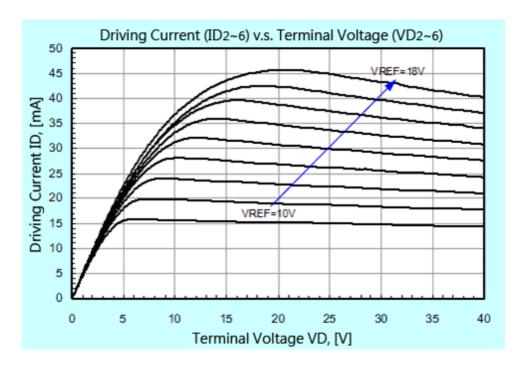


Figure 7: Driving current v.s. driver terminal voltage (I(D2..D6) v.s. V(D2..6))

To ensure DR3062's reliability, the current limiting driver is purposely desginged to have negative temperature coefficient to prevent "thermal-run-away". With negative temperature coefficient, the driver will lower the current when the driver's temperature rises; Lowering the driving current will, in turn, bring down the temperature; a safe thermal equilibrium is reached thus.



#### Supply current

The DC supply current to DR3062, IDC, is proportional to the external reference voltage as shown in Figure 8. For 110VAC/220VAC application, the power consumption is about 12mW/24mW with VREF being set at 18VDC.

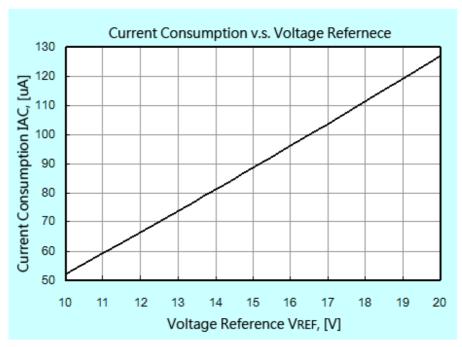


Figure 8: DC supply current v.s. reference voltage (IDC(VAC) v.s. VREF)

#### High Voltage LED Assembly

The high voltage LED consists of several low voltage LEDs in serial as shown below:

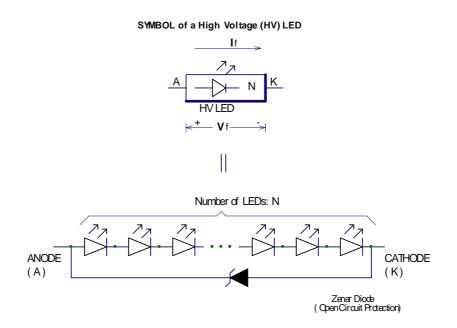
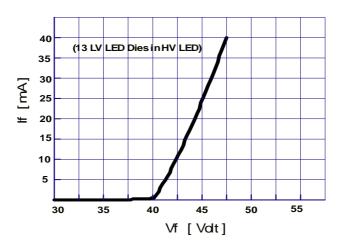


Figure 9: Assembly diagram of a high voltage LED



Since a high voltage LED is made by serially connecting several low voltage LEDs, the characteristics of the low voltage LED should be obtained first; the most important characteristics is the I-V curve. With the I-V curve, designers can calculate the number of low voltage LEDs required for building a high voltage LED. The I-V curve of a typical high voltage LED consisting of 13 low voltage LEDs is shown in Figure 3, the forward voltage is 47.5V when operating at 40mA.





If : forward current running through the HV LED Vf: forward voltage accross the HV LED

Fiure 10: IV Curve of a Typical High Voltage LED

#### How to calculate the number of lowe voltage LEDs (220VAC)

Design Parameters required:

• Rated input voltage: Vrated (unit: Vrms)

• Operating forward current: If (Uint: mA, considering main driving current I6 only)

• Forward voltage of LV LED at If: Vf (Unit: Vdc)

Total of LV LEDs required: Ntotal = Vrated \* 1.414 \* 0.9 / Vf (rounded to integer)

Case (1): Use 6 HV LEDs

The number of LV LEDs in each HV LED: Nhvled = Ntotal / 6 (rounded to integer)

Case (2): Use 7 HV LEDs (2 HV LEDs for the 1<sup>st</sup> driver)

The number of LV LEDs in each HV LED: Nhvled = Ntotal / 7 (rounded to integer)

Case (3): Use 12HV LEDs (2 HV LEDs for each driver)

The number of LV LEDS in each HV LED: Nhvled = Ntotal / 12 (rounded to integer)

Case (4): Use 13HV LEDs (3 HV LEDs for 1<sup>st</sup> driver, and two for the others)

The number of LV LEDs in each HV LED: Nhvled = Ntotal / 13 (rounded to integer)

#### Example:

The rated input power is 220VAC; the main driving current is set at 50mA. Assume that the forward volatge of LV LED is 3.65V when operating at 50mA, then the minimal number of LV LEDs required is: Ntotal = 220V \* 1.414\*0.9 / 3.65 = 77 (rounded to integer)

Case (1): Nhvled = 77 / 6 = 13 (rounded to integer)

Case (2): Nhvled = 77 / 7= 11 (rounded to integer)

Case (3): Nhvled = 77 / 12 = 6 (rounded to integer)

Case (4): Nhvled = 77 / 13= 6 (rounded to integer)



#### How to calculate the number of lowe voltage LEDs (110VAC)

Design Parameters required:

• Rated input voltage: Vrated (unit: Vrms)

• Operating forward current: If (Uint: mA, considering main driving current I6 only)

• Forward voltage of LV LED at If: Vf (Unit: Vdc)

Total of LV LEDs required: Ntotal = 2\*Vrated \* 1.414 \* 0.9 / Vf (rounded to even integer)

Case (1): Use 6 HV LEDs

The number of LV LEDs in each HV LED: Nhvled = Ntotal / 6 (rounded to integer)

Case (2): Use 8 HV LEDs (2 HV LEDs for the 1<sup>st</sup> driver)

The number of LV LEDs in each HV LED: Nhvled = Ntotal / 8 (rounded to integer)

Case (3): Use 12HV LEDs (2 HV LEDs for each driver)

The number of LV LEDS in each HV LED: Nhvled = Ntotal / 12 (rounded to integer)

Case (4): Use 14HV LEDs (3 HV LEDs for 1<sup>st</sup> driver, and two for the others)

The number of LV LEDs in each HV LED: Nhvled = Ntotal / 14 (rounded to integer)

#### Example:

The rated input power is 110VAC; the main driving current is set at 50mA. Assume that the forward volatge of LV LED is 3.65V when operating at 50mA, then the minimal number of LV LEDs required is:

Ntotal = 2\*110V \* 1.414\*0.9 / 3.65 = 78 (rounded to even integer)

Case (1): Nhvled = 78 / 6 = 13 (rounded to integer)

Case (2): Nhvled = 78 / 8= 10 (rounded to integer)

Case (3): Nhvled = 78 / 12 = 7 (rounded to integer)

Case (4): Nhvled = 78 / 14= 6 (rounded to integer)

#### **Heat Dissipation**

With the negative temperature coefficient of the six current drivers, DR3062C can operate in the condition of 125°C. However, a good heat dissipation design will not only reduce the accumulated heat but aso increase the LED's efficacy and life. The exposed thermal pad on the buttom of the package, desinged for maximizing thermal relief, must physically contact a heat sink on the PCB. The exposed thermal pad is electrically connected to GND terminal, therefore, it is not allowed to electrically connect to the metal housing.

#### The influence of Input Power Variation on Luminance

Although the DR3062 can drive the HV LEDs in the sense of constant current, the voltage variation of input power will affect the duty factor of each driving current, resulting in a variation on the light intensity. According to the field test results, when the voltage of input power drops 10% below rated voltage, the light intensity also drops 10%; when the voltage of input power increases 10% above rated voltage, the light intensity increases less than 5%. Both incandescent lamp or fluorescent lamp have the same phenominum. For human beings, 15% brightness change will not be noticed. Because DR3062 is not designed to work in constant power manner, when the electrical power drops, the current consumption will not increase. If the design of a large lighting system is based on constant power, the current will increase dramatically when the electricity is not able to supply enough power; in this case, the constant-power design will further deteriorate the power supply quality.

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#### Light switch with Neon Indicator

If a light switch with neon indicator is used, the neon indicator itself is a leakage path when the switch is turned off. In this case, the LED lamp might not be completely turned off. In this case, a  $47K\Omega$  resisor with 0805 package must be connected between the 1<sup>st</sup> driver terminal and VAC terminal to lower the voltage across the high voltage LED; alternatively, an X1 capacitor of 0.11uF is placed before the bridge rectifier to lower the voltage across the lamp. For details, please refer to application circuits.

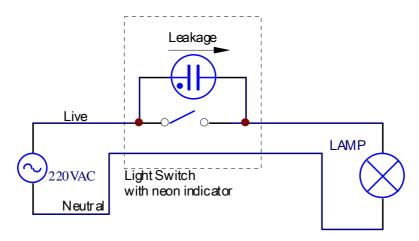


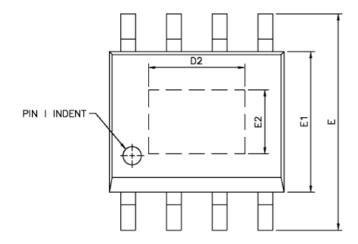
Figure 11: Light Switch with neon indicator

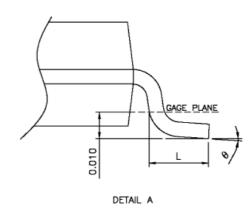
#### **Conformal Coating**

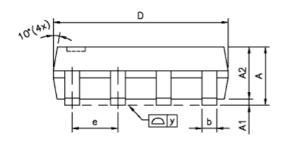
A conformal coating with the thickness of 30 ~120um should be applied to the printed wiring assembly in order to increase the air clearance and creepage distance between any two high voltage leads of DR3062. Conformal coating material is applied to electronic circuitry to act as protection against moisture, dust, chemicals, and temperature extremes that, if uncoated (non-protected), could result in damage or failure of the electronics to function. When electronics must withstand harsh environments and added protection is necessary, most circuit board assembly houses coat assemblies with a layer of transparent conformal coating rather than potting. The most common standards for conformal coating are IPC A-610 and IPC-CC-830. These standards list indications of good and bad coverage and describe various failure mechanisms such as dewetting and orange peel.

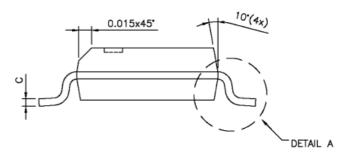


#### Mechanical dimensions of SOP8 Package









	EXPOSED PAD DIMENSION (inch)						
	PAD		D2		E2		
	OPTION SIZE	MIN	NOM	MAX	MIN	NOM	MAX
	A.)95x130mil	0.105			0.070		_
Λ	B.)90x90mil	0.065	—	_	0.065		

#### NOTE:

- CONTROLLING DIMENSION: INCH
  LEAD FRAME MATERIAL: COPPER 194
  DIMENSION "D" DOES NOT INCLUDE MOLD
  FLASH, TIE BAR BURRS AND GATE BURRS.
  MOLD FLASH, TIE BAR BURRS AND GATE BURRS
  SHALL NOT EXCEED 0.006"[0.15mm] PER END.
  DIMENSION "E1" DOES NOT INCLUDE INTERLEAD
  FLASH. INTERLEAD FLASH SHALL NOT EXCEED
  0.010"[0.25mm] PER SIDE
- FLASH. INTERLEAD FLASH SHALL NOT EXCEED 0.010"[0.25mm] PER SIDE.

  4. DIMENSION "b" DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.003"[0.08mm] TOTAL IN EXCESS OF THE "b" DIMENSION AT MAXIMUM MATERIAL CONDITION. DAMBAR CANNOT BE LOCATED ON THE LOWER RADIUS OR THE FOOT. MINIMUM SPACE BETWEEN PROTRUSION AND AN ADJACENT LEAD TO BE 0.0028"[0.07mm] ADJACENT LEAD TO BE 0.0028"[0.07mm]
- TOLERANCE: ±0.010"[0.25mm] UNLESS OTHERWISE SPECIFIED.
- 6. OTHERWISE DIMENSION FOLLOW ACCEPTABLE

	DIMENSIONS IN MILLIMETERS			DIMENSIONS IN INCHES		
SYMBOLS	MIN	NOM	MAX	MIN	NOM	MAX
Α	1.47	1.60	1.73	0.058	0.063	0.068
A1	0.10		0.25	0.004	_	0.010
A2	_	1.45			0.057	
ь	0.33	0.41	0.51	0.013	0.016	0.020
С	0.19	0.20	0.25	0.0075	0.008	0.0098
D	4.80	4.85	4.95	0.189	0.191	0.195
E	5.80	6.00	6.20	0.228	0.236	0.244
E1	3.80	3.90	4.00	0.150	0.154	0.157
е	_	1.27			0.050	
L	0.40	0.71	1.27	0.016	0.028	0.050
у	_		0.076			0.003
0	0,	_	8-	0.		8.



Appendix: Application circuit

110VAC application ( DR3062-SOP8-110) 220VAC application ( DR3062-SOP8-220) 240VAC application ( DR3062-SOP8-220)



