INTRODUCTION

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n many modern battery-powered electronic circuits, a DC supply is needed that is of either a larger voltage value than that of the main battery, or is of reverse polarity; a circuit that is powered from a six-volt battery may, for example, incorporate a single op-amp stage that needs +12V and -6V supply lines. In such cases, the required voltages may be generated via one or more special DC voltage converter circuits.

Ray Marston explains DC voltage converter operating principles and presents a selection of practical application circuits.

Most electronic DC voltage converters operate in one or another of four basic ways and use a DC-powered oscillator to drive either a simple diode-capacitor 'voltage multiplier' network, or a step-up transformer and rectifier network, or a 'flying capacitor' voltage converter, or a 'diode-steered charge pump,' which produces the desired final DC output voltage or voltages.

This article explains the operating principles of - and shows practical examples of - each of these four basic types of circuits.

DC 'VOLTAGE MULTIPLIER' CIRCUITS

BASIC PRINCIPLES

Conventional DC 'voltage multiplier' types of voltage converter circuits are based on a simple two-section diode-capacitor type of rectifier network that was originally designed way back in the 1930s for use in high-value AC-to-DC voltage conversion applications, and is still widely used today.

To understand this circuit's basic operation and terminology (which can sometimes be rather confusing), it is necessary to start off by looking at a simple AC-to-DC power conversion circuit, as follows:

The simplest AC-to-DC power conversion circuit is the basic halfwave rectifying type shown in Figure 1, which depicts a circuit that uses a transformer with a secondary voltage value of 250V rms.

Here, the AC voltage applied to the input of rectifier D1 swings alter--353V in the negative half-cycle.

DC VOLTAGE CONVERTER CIRCUITS <u>by Ray Marston</u>

biased during each positive half-cycle and thus charges capacitor C1 to a peak value of (ignoring D1's forward volt drop) +353V, but is reversebiased during each negative halfcycle, which thus has no practical effect on the circuit.

This circuit produces a positive output voltage, but can be made to generate a negative output voltage by simply reversing the polarities of D1 and C1.

The really important thing to note about the Figure 1 half-wave rectifier circuit is that D1 and C1 act together as a peak-voltage detector that makes the circuit give an output

a simple two-section 'voltage multiplier' circuit to do this job. Figure 2 shows such a circuit, driven from the secondary winding of a 250V transformer.

Here, the C1-D1 section acts as a diode clamp that, when fed with a normal AC input that swings symmetrically about the OV value, produces an output waveform that is of identical shape, but has its peak negative point clamped to the OV 'reference' value, as shown in the diagram.

This waveform's peak output value equals the peak-to-peak (Vp-p) value of the AC input voltage, and is fed directly into the input of the sim-

This circuit thus

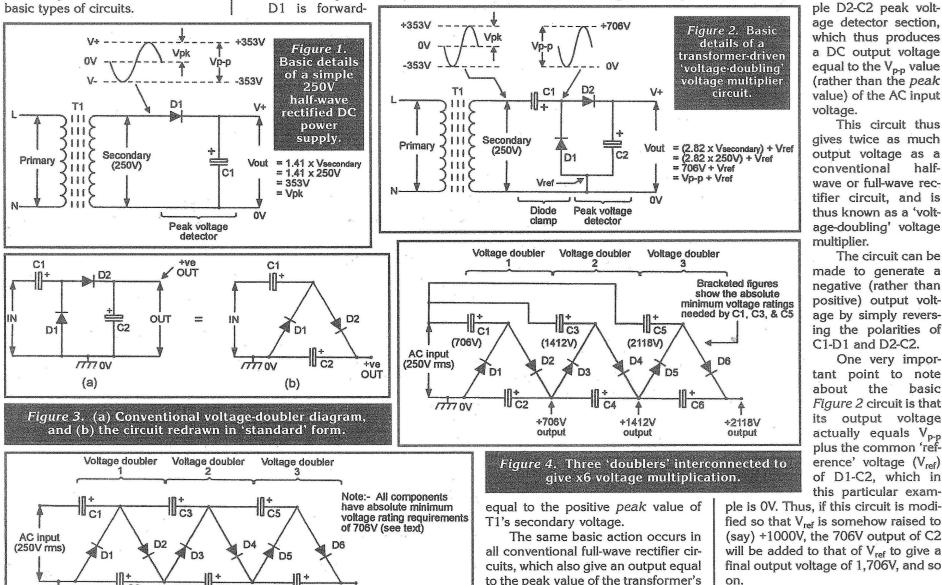
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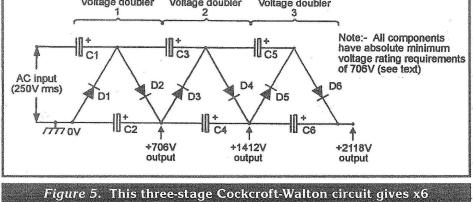
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The heart of the Figure 2 circuit is the actual C1-D1-D2-C2 voltage doubler network. Figure 3(a) shows the conventional diagram of this network and Figure 3(b) shows it redrawn as a 'standard' voltage-

nately above and below the OV value, rising to a positive V_{peak} (Vpk) value +353V in the positive half-cycle, and falling to a negative Vpeak value of D1 is forward-



voltage multiplication.

to the peak value of the transformer's secondary voltage.

During the early 1930s, engineers needed a cheap, reliable, and safe way of generating high-value low-power DC voltages from low-cost non-lethal transformers, and devised

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doubling voltage multiplier section.

A major feature of the voltagedoubler is that numbers of 'doublers' can easily be interconnected to give various values of voltage multiplication, and such circuits are best drawn by using the standard *Figure 3(b)* representation.

Figure 4, for example, shows three of these 'doubler' stages interconnected to give a voltage sextupler action in which the final output voltage is six times greater than the peak value of the original 250V rms input voltage.

Here, each 'doubler' section generates an individual output (across its C2, C4, or C6 capacitor) of 706V, but the output of the first doubler acts as the V_{ref} point of the second doubler, and the output of the second doubler acts as the V_{ref} point of the third doubler, the net effect being that the three individual output voltages add together to give a final DC output of +2118V from the 250V AC input.

Note in the *Figure 4* circuit that the input capacitor of each section is fed directly from the AC input voltage, and needs an absolute minimum voltage rating equal to that section's output-to-ground voltage, e.g., C5 needs a minimum rating of 2118V.

In the mid 1930s a modified version of the voltage multiplier was designed to overcome this snag. Known as the Cockcroft-Walton voltage multiplier, it uses standard voltage-doubler stages interconnected in the manner shown in *Figure 5*.

This circuit is similar to that of *Figure 4*, except that the input of each doubler (except the first) is fed from the 'clamped' AC voltage point of the preceeding doubler.

Consequently, the 'minimum voltage rating' requirement of each component used in each doubler stage equals the peak-to-peak value of the original AC input voltage.

A weakness of the Cockcroft-Walton voltage multiplier is that its output impedance is rather high (it is proportional to the sum of the impedances of the various input capacitors), and it can thus supply only small output currents.

In practice, this type of voltage multiplier was originally designed simply to generate a very high (up to about 30KV) accelerator voltage on the final anode of cathode-ray tubes, an application which requires very little energizing current.

Note that a 10-stage circuit of this type — when driven by a 500V AC input — generates a DC output of over 14KV, but the components used in each stage have minimum voltage rating requirements of less than 1.5KV.

PRACTICAL CIRCUITS

A DC voltage can easily be converted into one of greater value or of reversed polarity by using the DC supply to power a free-running 1KHz to 30KHz squarewave generator that **106** January 1998/Nuts & Volts Magazine

has its output fed to a voltage multiplier of one of the basic types already described, which thus provides the desired 'converted' DC output voltage. *Figure 6* shows a practical demonstration circuit of this type.

The Figure 6 circuit uses a type-555 'timer' IC (which can supply fairly high output currents) as a free-running squarewave generator that operates at about 3KHz (determined by the R1-R2-C2 values), and directly drives the C3-D1-D2-C4 'doubler' stage, which (ideally) produces a DC output equal to the peak-to-peak output of the squarewave, which (ideally) equals the Vcc value.

In practice, the squarewave's peak-to-peak value is slightly less than Vcc, and the 'doubler' loses another 1.2V in volt-drops in D1 and D2, the net result being that the actual output (when very lightly loaded) is about 1.6V less than Vcc, e.g., 8.4V with a 10V supply. The circuit can use any supply in the range 5V to 15V.

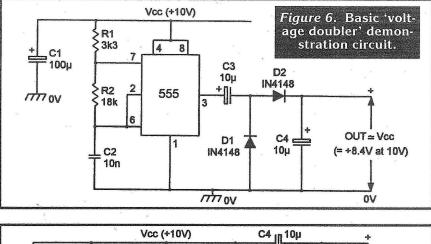
Figure 7 shows a far more useful version of the basic *Figure* 6 'voltage-doubler' circuit.

In this version, the C3-D1-D2-C4 'doubler' is tied to the positive (rather than 0V) supply line, and its output voltage is thus added to that of the supply line, thus giving a DC output voltage (when lightly loaded) of almost two times Vcc.

In practice, the prototype circuit gives an output of almost 19V when using a 10V supply.

Figure 8 shows the Figure 7 circuit modified for use with a cascaded pair of 'doubler' stages, in a configuration that is known (because it generates a DC output four times greater than a basic *peak* AC input voltage) as a 'voltage quadrupler.'

Here, the output of the new C5-D3-D4-C6 'doubler' stage (which is a couple of volts less than Vcc) is



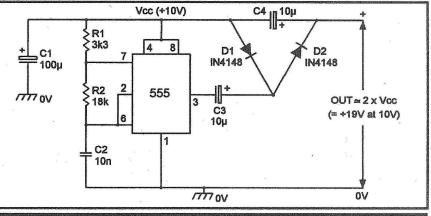


Figure 7. DC voltage-doubling circuit.

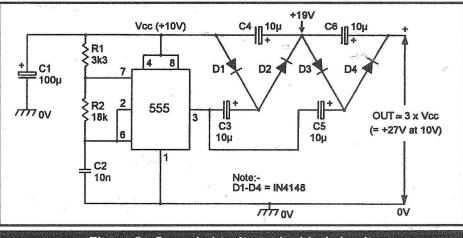
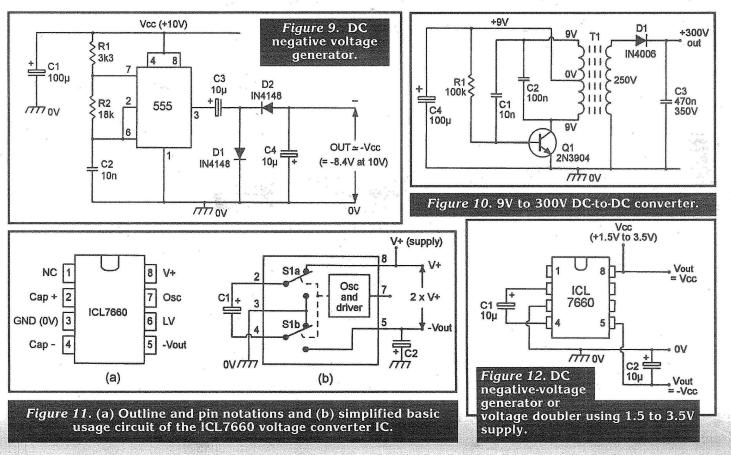


Figure 8. Cascaded 'voltage doubler' circuit.



added to that of the basic Figure 7 circuit, thus giving a DC output voltage (when lightly loaded) of almost three times Vcc.

In practice, the prototype circuit gives an output of 27V when using a 10V supply.

Figure 9 shows a particularly useful type of voltage multiplier circuit that generates a negative output voltage that (ideally) is almost equal

MOV

Figure 17. Method of reducing

oscillator frequency.

8

5

ICL

7660

VO TTT

in amplitude, but opposite in polarity

to that of the IC's supply line, thus

providing a split-supply output from

Vcc (+3.5V to 10V)

1k0

C2 5

10µ

Figure 19. External clocking of the ICL7660.

C2

10u

Vout = -Vcc

CMOS gate

VO TTT

Vout = -Vcc

Clock

input

inter and

a single-ended input.

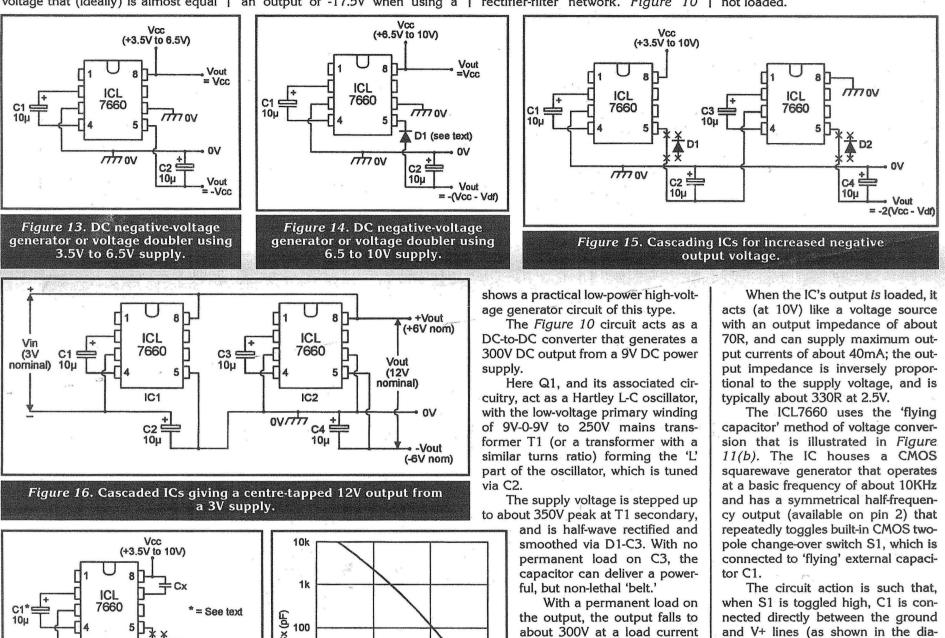
The circuit is similar to that of Figure 6, but has its D1-D2-C4 'doubler' polarities reversed, so that its output voltage is negative to the OV line.

In practice, the prototype circuit gives an output of -8.4V when using a 10V supply. (Note: two of these 'doubler' stages, when cascaded, give an output of -17.5V when using a

when hundreds of volts must be generated via a 6V to 12V supply), it is often better to use the output of a low-voltage oscillator or squarewave generator to drive a step-up voltage transformer, which then provides the required high-value voltage (in AC form) on its secondary (output) winding; this AC voltage can easily be converted back to DC via a simple rectifier-filter network. Figure 10 between pins 8 and 5.

The IC can thus be used as either a negative-voltage generator or as a voltage doubler.

The ICL7660 can be used with any +1.5V to 10V DC supply, consumes a typical quiescent current of 170µA at 10V, and has a typical +ve to -ve voltage conversion efficiency of 99.9 percent when its pin 5 output is not loaded.



(L) 100 10

> 10Hz 100Hz 1kHz 10kHz Oscillator frequency

Figure 18. Cx versus oscillator frequency graph.



A HIGH-VOLTAGE GENERATOR CIRCUIT

The 'voltage multiplier' method of generating increased values of DC output voltage is usually cost-effective only when multiplier ratios of less

ratios are required (as, for example,

than six are needed.

In cases where very large step-up

'FLYING CAPACITOR' DC VOLTAGE CONVERTERS

of a few milliamps.

One very efficient way of obtaining good +ve to -ve lowvoltage conversion is to use the so-called 'flying capacitor' technique, which is used by

the popular ICL7660 dedicated voltage converter IC (and its SI7660, LMC7660, etc., equivalents) and by several similar devices.

The ICL7660 is housed in an eight-pin DIL package as shown in Figure 11(a), and is designed to be powered from a single-ended DC supply that is connected between pins 8 (V+) and 3 (GND or 0V), and to generate an equal-value negative output on pin 5 (-Vout), i.e., if powered from a +5V supply, it generates a -5V output on pin 5, thus making double the supply voltage (i.e., 10V) available and V+ lines (as shown in the diagram) and thus charges up to the full positive supply voltage value.

On the next clock cycle, however, S1 toggles low and, under this condition, C1 is connected - in reverse polarity - directly across external output capacitor C2, thus generating an output voltage of V- across C2. This toggling sequence repeats continuously, at half of the clock-generator frequency.

Note that, since the ICL7660 uses CMOS rather than bipolar semiconductor switches in its 'conversion' circuitry, the IC operates with very high-voltage conversion efficiency.

The ICL7660 is an easy device to use, but none of its terminals must ever be connected to a voltage greater than V+ or less than GND (0V).

If the IC is to be used with supplies in the range 1.5V to 3.5V, the pin 6 'LV' terminal (which controls an internal voltage regulator) should be grounded; at supply values greater Nuts & Volts Magazine/January 1998 107 than 3.5V, pin 6 must be left open circuit. At supply values greater than 6.5V, a protection diode must be wired in series with OUTPUT pin 5.

The circuits of Figures 12 to 20 show a selection of practical designs in which these rules are applied.

ICL7660 CIRCUITS

ed in the same way as the right-hand IC of this diagram.

It has already been pointed out that a single ICL7660 IC can be used as a highly efficient voltage doubler that can, for example, generate a centre-tapped 10V output when powered from a single-ended 5V input. Figure 16

doing this is to wire capacitor Cx between pins 7 and 8, as in Figure 17; Figure 18 shows the relationship between the Cx and frequency values; thus, a Cx value of 100pF reduces the frequency by a factor of 10, from 10KHz to 1KHz; to compensate for this 10:1 frequency reduction

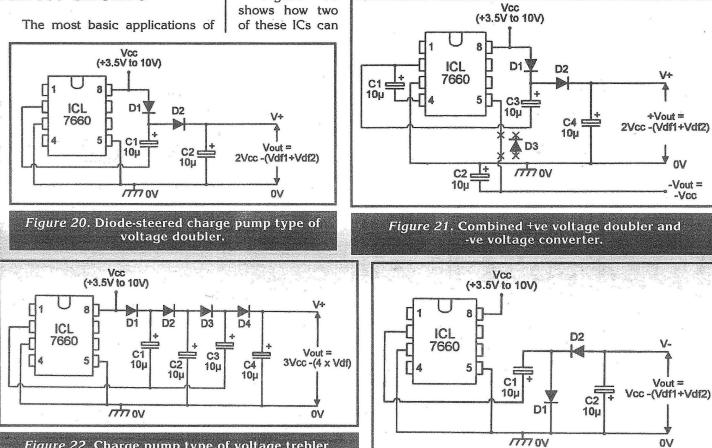


Figure 22. Charge pump type of voltage trebler.

the ICL7660 are as a simple negativevoltage generator or as a voltage doubler, and Figures 12 to 14 show three simple circuits of this type; in each case, C1 is a 'flying' capacitor and C2 is a smoothing/storage capacitor and each have a value of 10µF.

The Figure 12 voltage converter is intended for use with 1.5V to 3.5V supplies, and requires the use of only two external components.

The Figure 13 circuit is similar, but is meant for use with supplies in the 3.5V to 6.5V range and thus has pin 6 grounded.

Finally, the Figure 14 circuit is meant for use with supplies in the range 6.5V to 10V, and thus has diode D1 wired in series with output pin 5, to protect it against excessive reverse-biasing from C2 when the power supplies are removed. The presence of this diode reduces the available output voltage by V_{df} , the forward volt drop of the diode; to keep this volt drop to minimum values, D1 should be a germanium or Schottky type.

A useful feature of the ICL7660 is that numbers of these ICs (up to a maximum of 10) can be cascaded to give voltage conversion factors greater than unity. Thus, if three stages are cascaded, they give a final negative output voltage of -3Vcc, etc. Figure 15 shows the connections for cascading two of these stages; any additional stages should be connectbe cascaded to generate centrea tapped 12V output

when the circuit is powered from a single-ended 3V source (e.g., from two series-connected 1.5V cells).

Here, IC1 is used as a basic voltage doubler, powered from a 3V source connected between pins 3 and 8, and its 6V output (from between pins 5 and 8) is used to power IC2 via pins 3 and 8, and IC2 thus generates an output (between pins 5 and 8) of 12V when very lightly loaded. This 12V output has a source impedance of about 500R, and falls by about 0.5V per mA increase in load current (most of this volt drop is reflected from the -ve output of IC1, which operates at a current level two times greater than the IC2 output, as explained below).

It is important to note that the supply (battery) current consumed by any voltage multiplier circuit is inevitably at least n times greater than the circuit's loaded output current, where n is the circuit's 'multiplier' value. Thus, if a voltage doubler is powered from a 5V supply and generates a 10V x 10mA (= 100mW) output, it follows that the supply current must be at least 20mA (= 100mW/5V).

The circuit's output impedance is also proportional to the n value.

In some applications, the user may want to reduce the oscillator frequency of the ICL7660 IC; one way of and maintain the circuit efficiency, the C1 and C2 values should be increased by a similar factor (to about 100µF each).

Figure 23. Diode-steered charge pump negative-

voltage generator.

Another way of reducing the oscillator frequency is to use pin 7 to over-drive the oscillator via an external clock, as shown in Figure 19.

The clock signal must be fed to pin 7 via a 1K0 series resistor (R1), and should switch fully between the two supply rail values; in the diagram, a CMOS gate is wired as an inverting buffer stage, to ensure such switching.

DIODE-STEERED CHARGE PUMP CIRCUITS

So far, this article has described three of the four most widely used types of DC voltage conversion circuit.

The fourth type of converter is sometimes known as a 'diode-steered charge pump' circuit, and Figure 20 shows an example of one of these 'pumps' used in conjunction with an ICL7660 IC to make a converter that gives a positive output voltage of almost double the original supply voltage value.

The pump consists of D1-C1-D2-C2, and is driven by the low-impedance squarewave output of pin 2 of the IC. The circuit action is very

simple, as follows:

When the pin 2 output of the ICL7660 is switched low, it connects the low end of C1 to the OV line, so C1 charges to almost the full Vcc value via forward-biased diode D1. When the pin 2 output switches high

again, it pulls the low end of C1 up to Vcc, thus driving the top end of C1 up to almost double the Vcc value, thus reverse-biasing D1 and forward-biasing D2, and forcing C1 to dump its excess charge into C2, which thus charges up to almost double the Vcc value.

This process repeats continuously, with C1 automatically replacing any charge currents that are withdrawn from C2 by external loading circuitry. In practice, diodes D1 and D2 reduce the available output voltage by an amount equal to their combined forward volt drops, so they should ideally low-loss germanium or be Schottky types.

This 'charge pump' type of circuit is far more powerful than a conventional capacitor-diode voltage-doubler circuit, and can easily supply 10s of milliamps of output current.

Finally, to complete this look at DC voltage converter circuits, Figures 21 to 23 show three useful variants of the basic 'charge pump' circuit.

Figure 21 shows how the charge pump circuit of Figure 20 can be combined with the standard ICL7660 negative-voltage generator circuit of Figure 13 or 14 to

make a combined positive voltage multiplier and negative voltage converter that provides dual output voltage rails from a single-ended input supply.

Figure 22 shows how two of the Figure 20 type diode-steered charge pumps can be cascaded to make a voltage trebler that gives a positive output voltage that has an unloaded value equal to three times the Vcc voltage, minus the value of the seriesconnected diode volt drops. Typically, the circuit gives an output of about 27V when powered from a 10V supply.

Additional D3-C3-D4-C4 stages can be cascaded by wiring the low end of each odd-numbered capacitor to pin 2 of the IC, and the low end of each even-numbered capacitor to the OV line; each new stage increases the available output voltage by Vcc minus two diode volt drops.

Finally, Figure 23 shows a diodesteered charge pump negative-voltage generator circuit, in which diode and capacitor polarities are simply reversed and referenced to the OV line.

This circuit (when using ordinary silicon diodes) gives a typical unloaded output voltage of only -8.8V when powered from a 10V supply, but gives far better voltage regulation than a conventional ICL7660 negative voltage generator circuit. NV